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Deterioration Assessment of Infrastructure Using Fuzzy Logic and Image Processing Algorithm

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Balasubramanian Esakki⁴; and Rishi Gupta⁵

Abstract: The safety and serviceability of civil infrastructures have to be ensured either as part of a periodic inspection program or immediately following a given hazardous event. The use of digital imaging techniques to identify the deformed or deteriorated surfaces of structures is a substantial area of research and aims to investigate a number of unknown parameters, including damage quantification and condition rating. This manuscript illustrates the integration of previously developed fuzzy logic-based decision-making tools with the currently developed image processing algorithm to quantify the damage for the condition rating of civil infrastructures. The proposed integrated framework exploits visual specifics of different elements of the infrastructure to perform automated evaluation of structural anomalies such as cracks and surface degradation. Two different image segmentation tools, (1) bottom hat transform and (2) hue, saturation, color (HSV) thresholding, are applied to identify the surface defects. The developed image processing software is used with the fuzzy set framework proposed in the previous research to gauge the damage indices due to various deterioration types like corrosion, alkali aggregate reaction, freeze-thaw attack, sulfate attack, acid attack or loading, fatigue, shrinkage, and honeycombing. Case studies of a long-span bridge and a warehouse building are illustrated for concept validation. The refined comprehensive method is presented as a graphical user interface (GUI) to facilitate the real-time condition assessment of civil infrastructures. DOI: 10.1061/(ASCE)CF.1943-5509.0001151. © 2018 American Society of Civil Engineers.

Author keywords: Image algorithms; Fuzzy set framework; Deterioration; Structural health monitoring; Graphical user interface (GUI); Structural condition damage index (SCI).

Introduction

Civil structural health monitoring (SHM) has become an important requisite for diagnosis of material conditions and structural integrity as a whole to ensure the safety of critical civil infrastructures (Chang et al. 2003). It involves the condition assessment of civil infrastructures such as bridges, heritage structures, dams, power plants, pipelines, and other offshore structures. SHM is an efficient tool that can provide early warnings not only to safeguard the structures but also for the safety of end users. SHM can serve as an important tool to facilitate periodic infrastructure inspections. In many parts of the world, civil infrastructure is under tremendous strain because of increased traffic loads; shortened construction time; and lack of resources for inspection, maintenance, and repair of structures. Moreover, inspection of civil infrastructures after natural calamities, hurricanes, tornados, and fire can also greatly benefit from innovative SHM techniques. The sudden collapse

of structures, including bridges, can cause a high number of casualties. In these circumstances, SHM can be an invaluable tool to manage and maintain structural integrity and also guarantee the residual capacity of civil structures. Acquired knowledge on the condition of the structure through SHM paradigms will enable preventive measures to avoid catastrophic failures, leading to prolonged service life and ultimately reducing lifecycle cost. Structural evaluation in terms of strength, serviceability, and durability offers awareness to users and the public for maintenance, repair, rehabilitation, and decommissioning. The accumulated information can be maintained in a database that can help in formulating design guidelines for effective condition monitoring. One of the components of SHM is continuous monitoring using sensors and their related smart software (Dong et al. 2003). The present study describes the development of a graphical tool inculcating a fuzzy-system and image-processing module for appropriate estimation of the structural damage condition index (SCI). The collected information can be used as a database to formulate design guidelines for effective condition monitoring.

The initial sections of this paper describe the use of fuzzy logic developed by Jain and Bhattacharjee (2012a, b) for decision making and later to assess the damage indices for various structural defects such as corrosion, alkali aggregate reaction, sulfate attack, acid attack, fatigue, shrinkage, and honeycombing. A list of other deterioration mechanisms (along with their possible causes) not covered by this model can be found in the Portland Cement Association (PCA) guidelines (Portland Cement Association 2002). The more detailed findings presented in this paper are a result of integrating image algorithms with the fuzzy logic-based decision-making protocol that can be used to expedite the overall SHM process through automatic detection of multiple defects such as cracks, efflorescence, and other surface degradation, as shown in Fig. 1.

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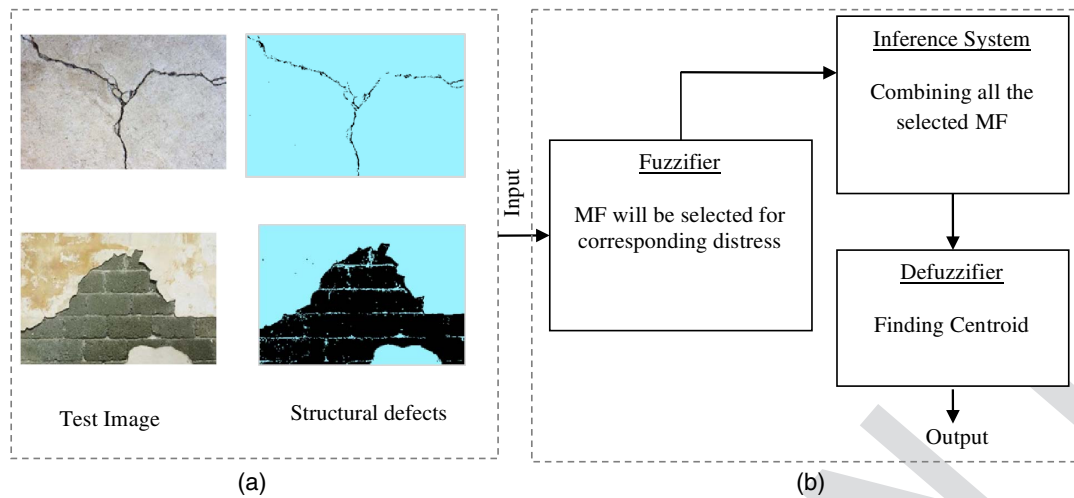


Fig. 1. Integration of image processing tool with the fuzzy logic framework for decision making: (a) image analysis; (b) fuzzy concept

Recent trends in digital acquisition and image analysis are becoming a pivotal factor in nondestructive testing of civil structures (Yao and Pakzad 2012; Jahanshahi and Masri 2012). Novel digital protocols can bring radical advances over conventional strategies and expedite overall inspection activity significantly (Sankarasrinivasan et al. 2015; Jahanshahi et al. 2009). Such innovative protocols provide essential support for proficient monitoring and diagnosis activities. To establish such automated systems, the development of sophisticated image processing tools is the foremost requisite in assessing critical infrastructural defects. The authors believe that the developed software module can facilitate image-oriented or image-assisted evaluation and corresponding structural damage assessment with reduced uncertainty brought in by human judgment. The main objective of this manuscript is to demonstrate the development and application of this image-based software module for inspection of the civil infrastructure.

Fuzzy Approach for Condition Assessment of Structures

A fuzzy logic framework is an artificial intelligence technique to provide solutions to solve complex problems using linguistic terms (Mamdani and Assilian 1975). It involves the development of membership functions (MFs), fuzzy logic actions, and defuzzifications. MFs are used to characterize the fuzzy set based on whether the selected elements are discrete or continuous in representing a graphical form with an essence of fuzziness. MFs are classified into triangular, Gaussian, trapezoidal, and Z shaped. In general, triangular MFs are widely used because of their simplicity in constructing fuzzy sets (Zhao and Bose 2002). After selecting appropriate MFs, the relationship between input and output parameters is formulated by a set of linguistic statements called fuzzy rules, and normally IF-THEN rules are adopted. The number of fuzzy rules corresponds to the number of fuzzy sets for each input variable. The evaluation of conditional statements occurs in parallel to tune the system in a random manner. The assessed fuzzy rules are used to provide an output for any input within the range of the fuzzy processes. However, an output of fuzzy inference needs to be a scalar quantity to determine the performance characteristics of the considered system. For this, defuzzification is carried out to convert the fuzzy values into a required output in which a fuzzy quantity is transformed into a precise quantity.

Few researchers have used fuzzy set theory (FST) for the evaluation of deterioration of civil structures. Blockley (1975, 1977) used FST to deal with structures failing because of causes other than stochastic variations in loads and strengths. Brown and Yao (1983) and Wang and Elhag (2007) used FST as a decision-making tool for the damage assessment of a structure and subsequent repairs. Similarly, researchers have dealt with similar topics, such as structural damage assessment (Ogawa et al. 1984; Souflis and Grivas 1986; Savage et al. 1988; Hathout 1993; Furuta et al. 2000; Liang et al. 2001), performance evaluation (Hadipriono 1988), expert systems for damage assessment (Ross et al. 1990), and condition assessment ratings (Arliansyah et al. 2003; Sasmal et al. 2006; Sasmal and Ramanjaneyulu 2008). Fwa et al. (2003) proposed a condition rating and maintenance need assessment system for airport pavement using fuzzy logic systems, which related distress conditions directly to maintenance needs. Kim et al. (2006) reported a FST-based assessment system for reinforced concrete (RC) building structures to estimate the current state of buildings and to provide guidelines for future maintenance and management.

Visual inspection of any deteriorating structure is an integral aspect of routine assessment practices. Data collected through visual inspection are primarily qualitative and subjective because they rarely involve precise measurements and depend heavily on expertise of the site inspection team. To deal with these concerns, Jain and Bhattacharjee (2012a, b) have proposed a methodology using fuzzy concepts for visual inspection-based condition assessment. They developed a tool using the Visual Basic application that can be accessed in Microsoft *Excel*. The present study uses this framework of fuzzy logic (FL) to obtain the structural condition index of civil infrastructures, and its working principles are outlined further subsequently.

In the context of condition assessment, fuzzy logic formulation is carried out initially by selecting MFs and the parameters to define these MFs are based on the user inputs as per the condition rating of structural elements. These MFs are further processed to account for the severity of deterioration occurring either as local or global in a structural element by using linguistic hedges or modifiers. However, elements of any structure have many distresses; hence, each has to be assigned appropriate MFs. The accumulation of MFs is obtained using the fuzzy weighted average technique. These combined MFs are evaluated using a set of fuzzy rules, normally IF-THEN rules, which are used further for assessing the condition

of the structure. In the present study, various codes are assigned for different distresses and severity levels, and they have been used to determine the damage conditions of an element. The conclusions drawn from these fuzzy rules are made available as crisp output to the user in the defuzzification process using the centroid method.

To prepare these MFs, a series of questionnaires were prepared related to commonly occurring distress manifestations (such as corrosion, delamination, poor workmanship, and acid attack) and distributed among professionals (experts) from the field of construction engineering. This work was carried out by Jain and Bhattacharjee. This rating varies from 0 to 5, where “0” represents a condition that does not require any repair and “5” represents critical conditions that require immediate action (Jain and Bhattacharjee 2012a). This study reported questionnaire responses from 26 practicing senior experts or consultants, 3 scientists, 22 academicians, and 15 international experts. However, the responses from individual experts seemed to differ because of varied perceptions in predicting the distress rates of the structure. Hence, these observations need to be incorporated in a systematic way through developing membership functions in FST.

In the present study, various response data from individual experts are captured by following multiple steps to develop MFs. The collected response data are appropriately assigned a condition rating and evaluated further. Initially, if the intermediate condition rating is smaller than predecessor and successor, then the average of these ratings is considered an intermediate rating. For example, $R_0, R_1, R_2, R_3, R_4,$ and R_5 are obtained as condition ratings, in which R_4 is lower than both R_3 and R_5 , and R_4 is revised as the average of R_3 and R_5 . In order to apply fuzzy set theory, the condition rating values should be in increasing order. Different condition ratings (R_0 to R_5) on the same structure are given based on the repair priority of the structure at once (no replicated inspections), as suggested in the literature by Mitra et al. (2010). In simple terms, experts could have different opinions on the same defects present in the structure or structural element. For example, a structure or structural element could be given any rating (R_0 to R_5) by an expert for the same deterioration mechanism or distress. Secondly, in order to neglect the small contribution of expert opinion in an evaluation of distress levels where the condition rating of the individual is less than the specific percentage of the summation of total respondents, then the same is updated to zero. A typical scenario where R_0 is less than a certain percentage (assume 10%) of summation of $R_0, R_1, R_2, R_3, R_4,$ and R_5 , means R_0 is updated to zero. Further, the condition ratings arrived at are normalized with respect to the peak number of responses. Later, the evaluated fractional values are considered as degrees of MFs (μ) corresponding to their condition ratings. The obtained MFs are modified using linguistic hedges and modifiers (Mitra et al. 2010) to account for local and global levels of defects, which are given by

$$\begin{aligned} \text{Local: } \mu_{x_i, \text{local}} &= \mu_{x_i}^{1/2} \quad \text{for } x_i \leq x_0 \\ \mu_{x_i, \text{local}} &= \mu_{x_i}^2 \quad \text{for } x_i \geq x_0 \end{aligned} \quad (1)$$

$$\begin{aligned} \text{Global: } \mu_{x_i, \text{global}} &= \mu_{x_i}^2 \quad \text{for } x_i \leq x_0 \\ \mu_{x_i, \text{global}} &= \mu_{x_i}^{1/2} \quad \text{for } x_i \geq x_0 \end{aligned} \quad (2)$$

where x_i = condition rating (0–5); and x_0 = condition rating where the MF is maximum.

The exponential term μ_x^2 involving the square of the MF values reduces the magnitude of the MF value at x . In contrast, $\mu_x^{1/2}$ increases the same. The use of modifiers ensures that if a certain severity of distress occurs “locally,” then distress would warrant

less repair action and “global” warrant higher repair action (Jain et al. 2012; Mitra et al. 2010).

The terms “local” and “global” are used in determining the extent of each distress and have been accounted by means of limits in the definition of membership functions. For example, the local extent will be considered if an element under study has $\leq 15\%$ damage. Global will be considered if the damage is present all over the area under study. The philosophy behind this is given in the literature by Mitra et al. (2010).

So far, MFs have been developed for various defects individually. However, any structural element can undergo more than one deterioration, and that has to be accounted for in evaluating the damage condition of civil structures. In view of this, each distress can be assigned applicable MFs, and a generalized fuzzy rule will be formulated. In order to account for the combination of defects, a combined MF has to be developed using the following steps. MFs are initially rescaled using the following relation:

$$x_i^{j'} = \frac{x_i^j}{a - x_i^j} \quad (3)$$

where $x_i^{j'}$ = scaled condition rating for the i th MF at the j th distress; x_i^j = unscaled condition rating for the i th MF at the j th distress; and a = spread of the universe of discourse ≈ 5 . To avoid any discontinuity, a has been assumed to be slightly greater than 5.0 (5.0001). As a user, you could select any value slightly greater (value $+ 1 \times 10^{-3}$) than the actual rating. If the actual rating value is used (in this case 5), then both a and x_i^j being 5 would render $x_i^{j'}$ mathematically undefined.

Further, by using the vertex method (Dong and Shah 1987), the scaled MFs are aggregated to obtain combined MFs as given by

$$\begin{aligned} \mu_i | x_i^{j'} \\ \text{for } \mu_i \in \{0, 0.1, 0.2, \dots, \dots, 0.9, 1.0, 1.0, 0.9, 0.8, \dots, \dots, 0.2, 0.1, 0\} \end{aligned} \quad (4)$$

where $x_i^{j'} = \sum_j x_i^{j'}$ = aggregation of MF on a modified scale.

Finally, the scaled MFs are reverted to the original scale using Eq. (5)

$$x_i^j = \frac{ax_i^{j'}}{1 + x_i^{j'}} \quad (5)$$

where x_i = original scale rating corresponding to the MF value μ_i .

After formulating the combined distress effects, defuzzification is carried out using the centroid method (Madau and Feldkamp 1996). The centroid is calculated based on the following formula:

$$\text{Centroid} = \frac{\sum_{i=1}^n \frac{1}{6}(x_{i+1} - x_i)(2x_i y_i + x_{i+1} y_i + x_i y_{i+1} + 2x_{i+1} y_{i+1})}{0.5(x_{i+1} - x_i)(y_i + y_{i+1})} \quad (6)$$

where x = condition rating; y = degree of MFs; and i = number of areas, which varies from 1 to n .

The resulting centroid represents the condition index of an element. Initially, this is performed for all the elements that correspond to an individual deterioration mechanism. Later, using the weighted average method, structural condition indices will be determined. In the weighted average method, each element condition index is assigned with a weight depending upon the significance of

251 an element. The ratio of summation of the weighed condition index
252 to the summation of weights is calculated as SCI to examine the
253 damage condition of the structure.

254 In order to understand more clearly the distress manifestation
255 conditions along with severity, a code is generated as deterioration–
256 distress–severity–extent. For example, CORR-CRACK-MOD-G
257 represents corrosion as deterioration, cracks as distress, severity
258 at a moderate level, and extent as a global level, similar to previous
259 work (Jain and Bhattacharjee 2012b). Similarly, MFs are generated
260 for all the inspection condition codes. Different deterioration mech-
261 anisms considered in this study are corrosion, alkali aggregate
262 reaction, freeze–thaw attack, sulfate attack, acid attack, fatigue,
263 shrinkage, and honeycombing. The detailed procedure for develop-
264 ing MFs is explained further in the Appendix.

265 Image Algorithm for Detection and Quantification of 266 Structural Defects

267 The formation of cracks is an early indication of deterioration,
268 especially in reinforced concrete structures. Cracks can lead to
269 reduction in the structural integrity of structures or catastrophic
270 failure if not assessed properly and regularly. The traditional crack-
271 monitoring methods are performed by professionals, and crack
272 patterns have to be located and sketched manually. Such detection
273 methods are laborious, time consuming, and subjective. In order to
274 accelerate the process, an image processing–based crack detection
275 method is suggested in this study and proven to be effective in
276 estimating surface defects.

277 Jahanshahi et al. (2009) explored a survey of vision-based crack
278 and corrosion detection approaches. Rose et al. (2014) reviewed
279 experimental systems to determine the cracks in concrete bridges.
280 Ikhlas et al. (2003) compared four crack detection techniques,
281 namely the fast Haar wavelet transform (FHWI), fast Fourier trans-
282 form (FFT), Sobel, and canny edge detectors. Yamaguchi et al.
283 (2008) and Yamaguchi and Hashimoto (2010) considered a scal-
284 able image processing method to analyze larger images. Prasanna
285 et al. (2012) proposed histogram-based feature extraction and a
286 statistical interference algorithm to identify the cracks. Lattanzi
287 and Miller (2014) exploited the intrinsic characteristics of images
288 through segmentation based on the canny and K-means methods.
289 Torok et al. (2014) reconstructed 3D profiles and subsequently
290 measured the geometrical characteristics, including cracks, of col-
291 lapsed building structures. Though crack detection algorithms are
292 predominantly successful, the quantification aspect is still chal-
293 lenging and dependent on many practical issues (Zou et al. 2012).
294 Limited research outcomes have been published, including mor-
295 phological filters (Nguyen et al. 2012), scanning electron mi-
296 croscopy (Vidal et al. 2016), and depth-perception techniques
297 (Jahanshahi and Masri 2013). In contrast to the prevailing literature,
298 the proposed methodology uses a rapid and computationally inex-
299 pensive inspection system that can be operative for both color and
300 grayscale images. This paper also highlights crucial parameters
301 for structural damage forecasts, such as crack length and surface
302 degradation.

303 In the subsequent section, an effective crack-detection algorithm
304 is formulated considering both the morphological and color fea-
305 tures of cracks. Hough-based filtration is adopted to eliminate
306 unnecessary edges that do not represent cracks. In addition, a quan-
307 tification of cracks is obtained based on the vision technique to
308 examine the criticality of the damage to the infrastructure. A study
309 has also been conducted to calibrate the developed model. The de-
310 scription of the proposed approach is given subsequently.

Morphological Approach

312 The morphological filter is widely used for the detection of struc-
313 tural patterns, feature analysis, and shape extraction from binary
314 and grayscale images. Because concrete cracks possess some dis-
315 tinct patterns, this paper proposes a specific morphological filter for
316 crack detection. In order to examine these characteristics, suitable
317 image filters are to be incorporated. Initially, the test images are
318 converted into grayscale, and the bottom hat transform is per-
319 formed. Then, images are skeletonized and the Hough line filter is
320 applied to remove the unnecessary regions. Finally, erosion and
321 postprocessing of the filtered images provide the quantification
322 of cracks. The detailed description of each morphological param-
323 eter is given subsequently.

Bottom Hat Transform (BHT)

325 BHT is a morphological filter capable of extracting image features
326 that are dark toned and satisfy specific structural geometry. The
327 mathematical expression is given by the difference of the image
328 and its closing by a structural element, as in Eq. (6)

$$B_{out} = (Img \ s) - Img \quad (7)$$

329 where Img and s = the test image and structural element, respec-
330 tively; and B_{out} is the output binary image. In a structure being
331 studied by the authors, the structural element matrix of 3×3 size
332 and the output correspond to pixel elements that are smaller in size.
333 In general, the size of the structural element has to be calibrated on
334 a par with acquisition parameters such as capturing distance and
335 resolution. In order to evaluate the proposed image algorithms,
336 various cracks on the walls are considered, which are shown in
337 Fig. 2(a).

338 Though the performance of the BHT is satisfactory, the results
339 obtained are often superfluous. They provide inaccurate informa-
340 tion in real-time scenarios where thin dark edges resulting from
341 wall curvature, door edges, and other corners of the structure appear
342 as cracks. The simulation results for a random test image [Fig. 2(b)]
343 using the BHT transform shows both cracks along with other erro-
344 neous dark edges or corners. Hence, it needs additional filtration to
345 remove the excessive edges other than cracks.

Skeletonization

347 This process is carried out to convert the detected edges into a sin-
348 gle pixel-wide line. During this process, redundant edge pixels are
349 removed, which assists in the appropriate segmentation. Because
350 the crack length quantization relies on a unique representation
351 of cracks, this step is, foremost, important in removing surplus
352 pixels. Once the skeletonizing is done, a Hough transform is ap-
353 plied to remove the edge segments that are perfectly straight.

Hough Line Elimination Filter

355 A Hough transform is a mapping of image pixels in the spatial (x, y)
356 domain to (r, θ) Hough space. Under such a transformation, the
357 presence of collinear points in the spatial domain is represented by
358 a point with a similar angle and distance in Hough space. The prob-
359 lem of classifying dark corners and edges from the detected cracks
360 is critical in crack quantification. Hence, this paper proposes the
361 application of a Hough transform to identify straight line edges.
362 Further, by setting a proper threshold, the unwanted edges can be
363 nullified in the output image. Hence, the straight line edges present

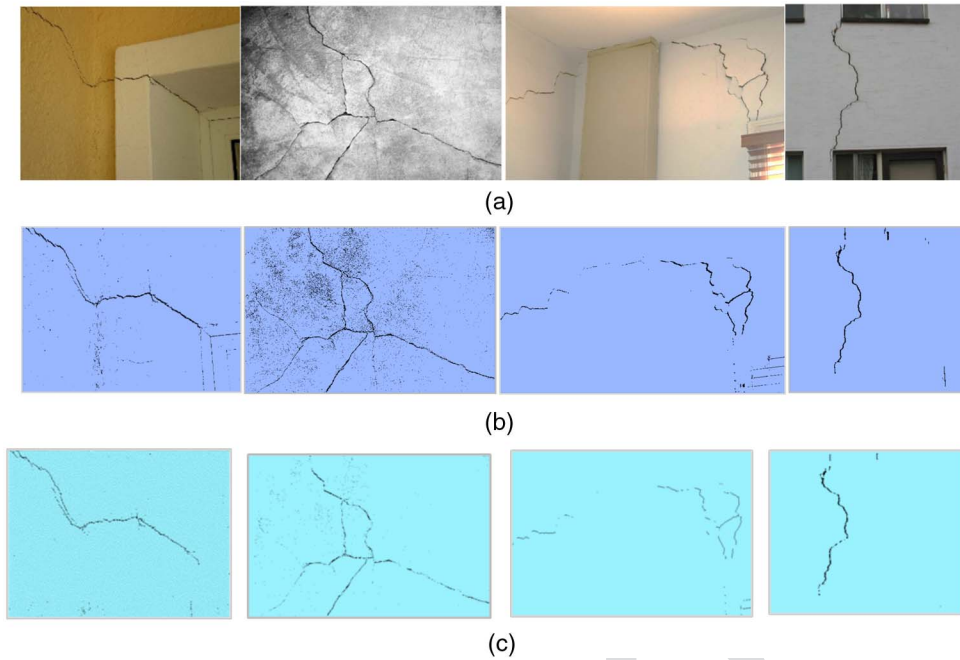


Fig. 2. Test images and detection of cracks (a) various cracks on the walls; (b) BHT transform output; (c) improved crack results

F2:1

364 in the output image can be eliminated by setting the proper
 365 threshold. Fig. 2(c) shows the output after incorporation of the
 366 Hough filter, where it can be clearly seen that all the straight line
 367 edges are removed except the cracks.

368 Erosion and Other Processing

369 Erosion removes all the insignificant regions that are negligible in
 370 relation to the detected segments. In particular, it is very effective
 371 in removal of isolated points and small regions that cannot be elim-
 372 inated by Hough and BHT filters [Fig. 2(c)]. Further processing
 373 consists of removing isolated points and maintaining continuity
 374 of the edge pixels.

375 Hue, Saturation, Color (HSV) 376 Thresholding—Color-Based Approach

377 In this approach, the color information of the test image is manip-
 378 ulated to discriminate crack pixels. The test images are converted
 379 from the red, green, blue (RGB) color space to the hue space for
 380 its robustness and accuracy. The HSV images are skeletonized, then
 381 a Hough line filter is applied to remove the unwanted regions.
 382 Further, erosion of images and postprocessing results in the quan-
 383 tification of cracks.

384 Extensive experiments have been conducted to derive the
 385 thresholding limit, and it has been found that cracks are

characterized by lower saturation and value in HSV space. The
 algorithm was tested for various test images, and the results shown
 in Fig. 3 confirm the detection of cracks.

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Quantification of Cracks

389

The data acquisition method and image protocols are of prime
 importance in quantifying cracks. The acquisition phase involves
 capturing images normal to the surface with an acquisition distance
 of 30–50 cm and an RGB image resolution of 640×480 pixels.
 A test database was created comprising 20 images with different
 crack lengths and widths. These images were taken during the eve-
 ning hours in fairly bright conditions.

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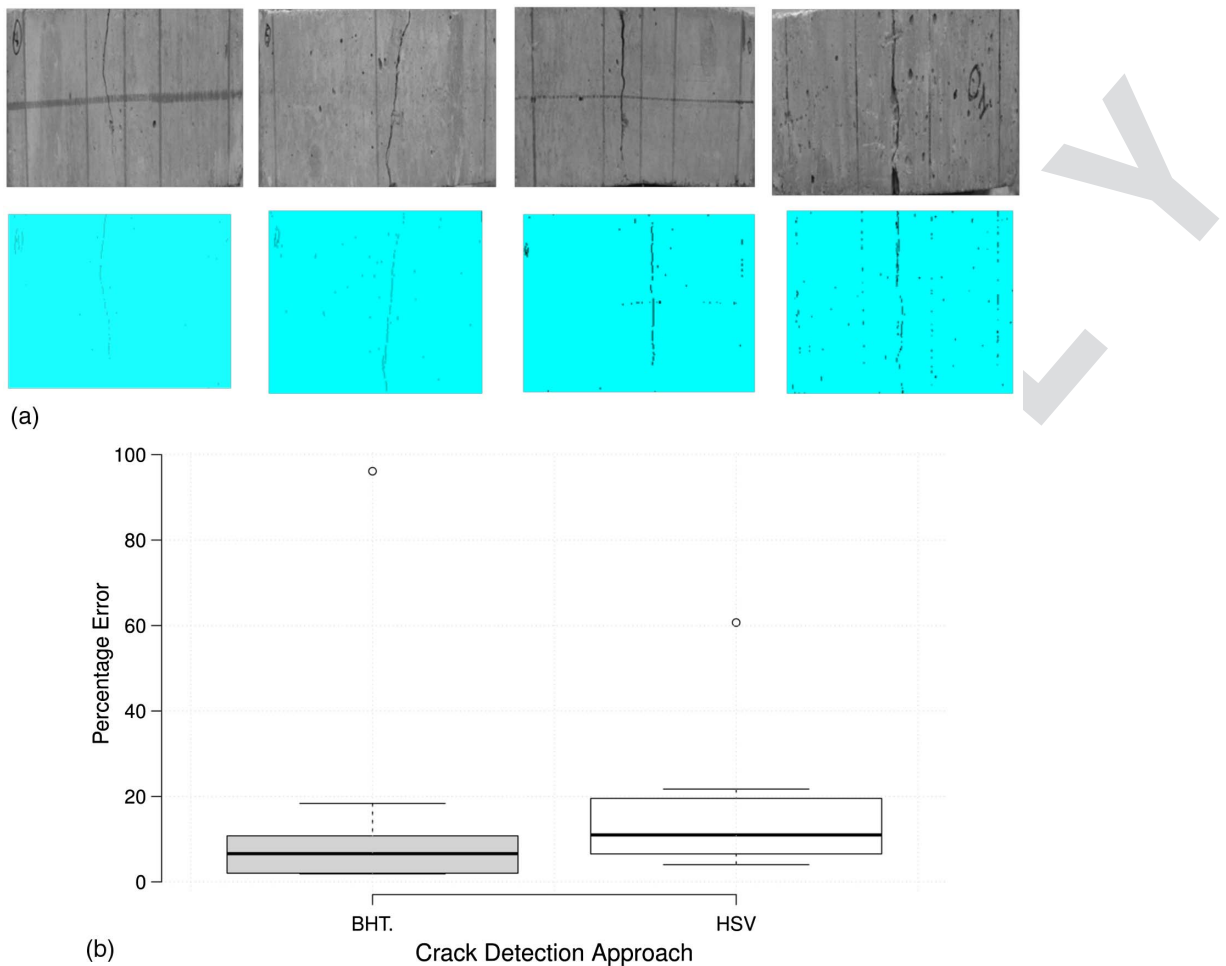
To validate the accuracy of the developed protocols, some of the
 sample database images are tested using the image segmentation
 approach to detect the edges of cracks and later used to find the
 crack width and length. In this approach, initially, the test images
 are converted into binary images. The cracks and void structures to
 be segmented should differ greatly in contrast from the background.
 The gradient and threshold of the test images have been calculated
 and applied to create a binary mask containing the segmented
 cracks and voids. In order to achieve these tasks, edge and Sobel
 operators have been used. Fig. 4(a) shows images of concrete
 prisms that have undergone flexural loading. There are black lines
 on the specimens that were drawn using black ink to facilitate po-
 sitioning of the specimens during testing. These drawn lines do not

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Fig. 3. HSV thresholding crack output

F3:1



F4:1 **Fig. 4.** (a) Image database of samples with different crack sizes; (b) percentage error for BHT and HSV approach in comparison with actual
 F4:2 measurements

410 represent any cracking. In addition, quantified crack lengths are
 411 given in Table 1.

412 The crack length is obtained by considering all the detected
 413 crack pixels (no linearity is assumed). For example, if there are
 414 N detected crack pixels (during calibration) where the distance
 415 between any pixels corresponds to x cm, then the overall N pixels
 416 corresponds to $(N - 1) * x$ cm. Therefore, the algorithm perform-
 417 ance depends on how effectively filters are performing the clas-
 418 sification, and from Fig. 4(a), it is obvious that detection effi-
 419 ciency is acceptable to obtain close to the actual value. The actual mea-
 420 sured length of cracks was obtained using a hand-held microscope.

421 In order to evaluate the overall performance of the developed
 422 algorithm, the whisker plots are provided (to show the overall
 423 percentage error), as shown in Fig. 4(b). It can be inferred from
 424 the plots that BHT and HSV perform with a percentage error of

10 and 20%, respectively. Hence, the structural-based approach is
 425 preferable for its exactness and eliminates detection of other surface
 426 degradations from cracks.
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428 Estimation of Surface Quality

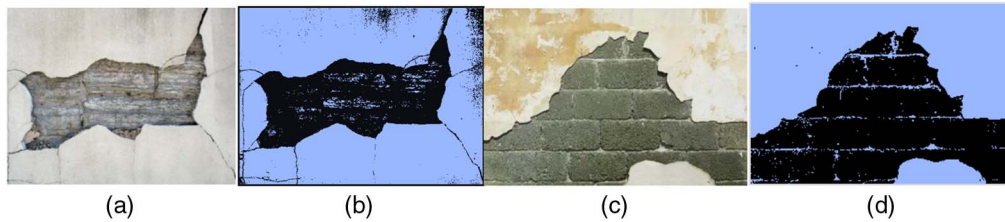
429 The other important aspect of assessing the quality of civil infra-
 430 structure is to estimate surface deterioration. Surface degradation
 431 is characterized by the formation of color patches or loss of outer
 432 layers, resulting in degradation of concrete or masonry surfaces.
 433 The primary cause is prolonged exposure to environmental load-
 434 ings such as heat, moisture, and chemicals. Histogram-based image
 435 thresholding has been proven to be an operative strategy to quantify
 436 surface deteriorations (Vázquez et al. 2011).

437 The proposed algorithm requires the user to select the unaf-
 438 fected area in a test image as an initial step. In the subsequent pro-
 439 cess, thresholding limits are automatically computed to classify the
 440 normal and degraded sections. The surface quality of images is as-
 441 sessed through histogram analysis after identifying the affected
 442 area from the grayscale of the test images.

443 The sample images shown in Figs. 5(a and c) are considered for
 444 the analysis. The processed images are shown in Figs. 5(b and d). It
 445 can be observed that the finishing layer (plaster surface) of the test
 446 surface is degraded and severely spalled. To estimate this degrada-
 447 tion, the histogram is applied on the test images, and the resulting

Table 1. Comparison Table for the Actual Crack Length Versus Algorithm Output

Image	Actual measured length of crack (in cm)	Number of crack pixels	Computed crack length (in cm)
T1:1	10	643	9.18
T1:2	12	872	12.457
T1:3	10.5	793	11.36
T1:4	10	1,022	14.6



F5:1 **Fig. 5.** Surface quality assessment using the developed image processing tool: (a) test surface 1; (b) test output 1; (c) test surface 2; (d) test output 2

448 output images are shown in Figs. 5(b and d). The thresholding
 449 bounds are extracted from the user-indicated surface area [in
 450 Fig. 5(b)] as shown in Fig. 5(a). The damage area is computed
 451 in proportion to the image pixels belonging to the affected area.

452 Development of Graphical User Interface (GUI) and 453 Its Validation

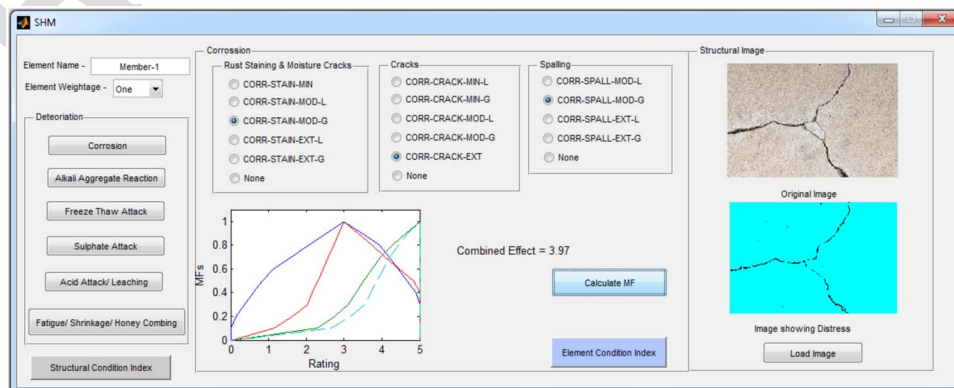
454 A user-friendly graphical interface has been developed using
 455 *MATLAB* functions to examine the structural condition of civil in-
 456 frastructures. This tool incorporates six structural deteriorations, as
 457 shown in Fig. 6, that are considered to be prominent for evaluating
 458 the health conditions of structures. For each deterioration, various
 459 surface defects are accounted for. For example, for corrosion, there
 460 are three different defects that are considered, as shown in Fig. 6,
 461 and in which the severity level of damage is rated as minimum
 462 (min), moderate (mod), and extensive (ext). The developed image-
 463 processing algorithm is integrated into the graphical user interface
 464 to quantify the crack and other surface defects. In addition, a fuzzy
 465 logic framework to generate MFs is also interfaced with the GUI,
 466 where the user can visualize the condition rating of structures. The
 467 combination of image processing and fuzzy logic algorithms provid-
 468 es an effective evaluation strategy of civil infrastructures. After
 469 selecting the deterioration and corresponding defects, the cumula-
 470 tive damage is assessed as an element condition index. The calcul-
 471 ated index value represents the criticality of the structure.

472 The designed GUI for SHM, as shown in Fig. 6, has two
 473 sections wherein fuzzy sets and image algorithms are inculcated.
 474 The first section takes into account the deterioration effects based
 475 on corrosion, alkali aggregate reaction, fatigue, shrinkage, honey-
 476 combing, acid attack, sulfate, and freeze–thaw attack. The other
 477 section computes the quantity and quality of the damage based on
 478 developed image algorithms. Captured images are loaded into the
 479 GUI using the “Load image” option, and, correspondingly, the

crack pattern, quantification of crack length, and quality of the sur-
 face are computed. The properties of cracks such as thin segmen-
 tation and random structural geometry are crucial to determine the
 length of the crack. Initially, a bottom hat transform filter is adopted
 to capture thin segmentation, dark nature, and random orientation.
 The unwanted edges are removed using a Hough-based filter. The
 standard library tools available in *MATLAB* are used to perform a
 bottom hat filter, Hough transform, and morphological operations
 such as erosion and dilation. In the case of detecting surface
 deterioration, a HSV-based filter technique is implemented. Initial-
 ly, the algorithm is trained with several images having known crack
 lengths and, accordingly, thresholding parameters and filter size
 are optimized. The training algorithm was further used for 20 images
 having varied crack lengths, and the results were found to be con-
 sistent with manual measurements. The processed and original im-
 ages are further helpful to identify the type of distress that has
 occurred, and they also can be used to identify global or local
 damage levels. Image-based distress estimation is further used to
 quantify the SCI. On the selection of appropriate distress levels
 and by clicking the “Calculate” button in the GUI, the intensity
 level of combined distress is automatically computed and the result
 displayed under “Combined Effect.” A sample calculation and the
 corresponding generation of MF are shown in Fig. 6.

503 Case Studies

504 In order to validate the developed tool for civil infrastructures,
 505 a southern railway bridge located at Manavur, Tiruvallur, and a
 506 storage building located near Avadi, Tamil Nadu, India, were se-
 507 lected as a case study. The discussion presented in this section
 508 is limited by a combination of some assumed damage initiation
 509 mechanisms and the available list of deterioration codes presented
 510 in previous studies.



F6:1 **Fig. 6.** SCI evaluation using developed tool; distress and selected MF are for demonstration purposes only

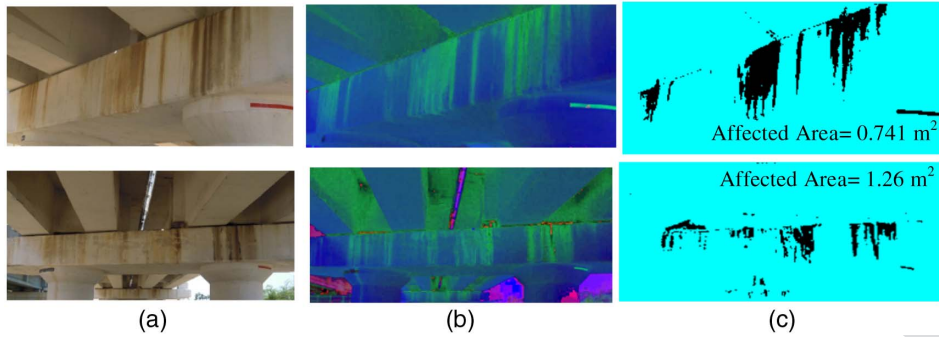


Fig. 7. Pier cap of railway bridge span 2 and 12: (a) site image; (b) HSV color space; (c) image showing distresses

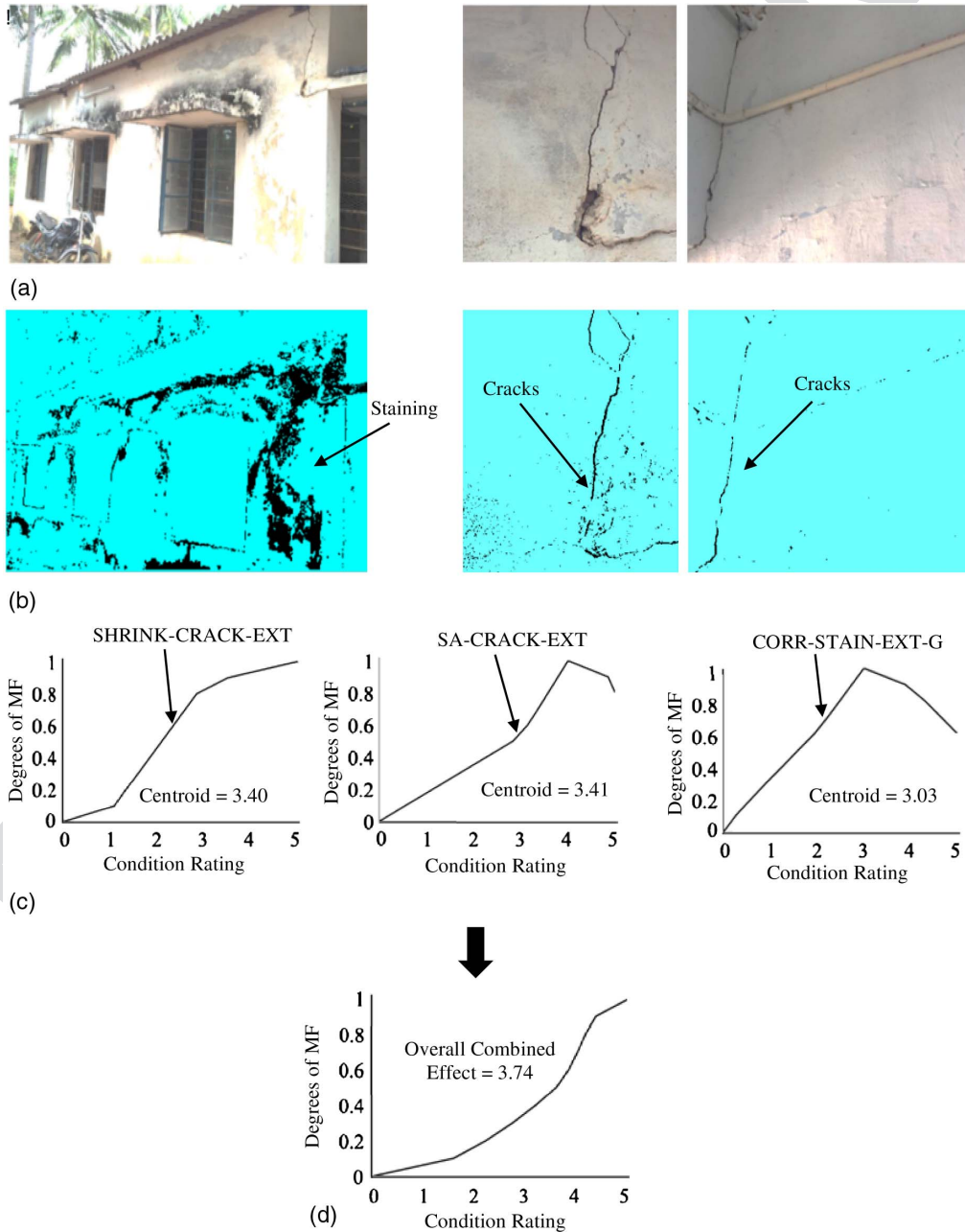


Fig. 8. East side wall of storage building: (a) unprocessed images; (b) corresponding distress-identified images; (c) effect for each deterioration; (d) overall damage index

F7:1

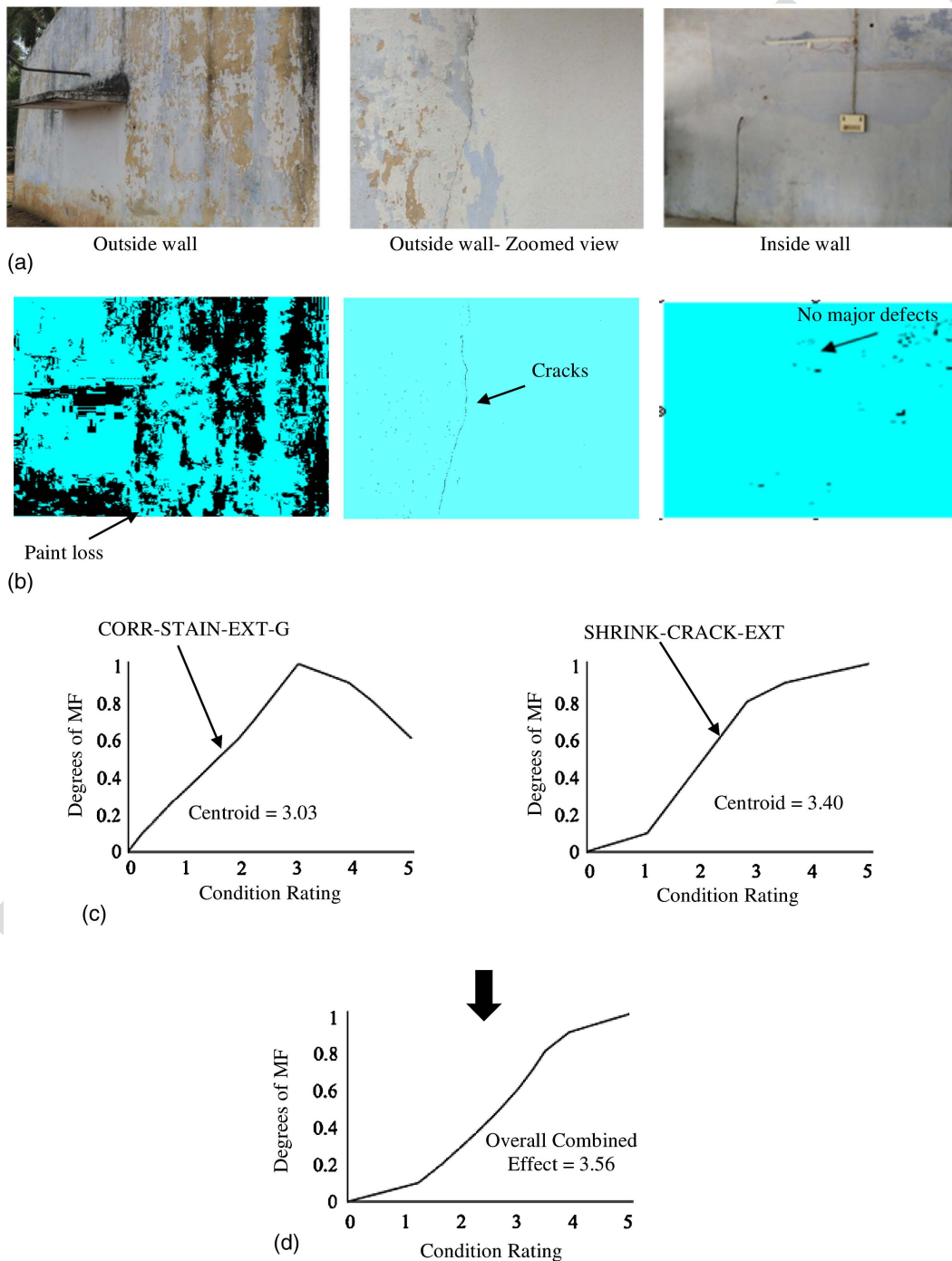
F8:1

F8:2

511 Digital images of bridge elements were captured, and it was
 512 found that no remarkable damage had occurred on load-bearing
 513 elements. However, the authors believe that this bridge has pre-
 514 dominantly been affected by heavy rain events and corrosion,
 515 which is the primary concern. Sample images shown in Fig. 7(a)
 516 were fed into the developed GUI, and the corresponding surface
 517 quality was evaluated, as shown in Figs. 7(b and c). At this stage,
 518 rather than relying completely on human judgment, the surface
 519 staining can be quantified using the image algorithms discussed
 520 earlier in this paper, and this value can be very useful in assigning
 521 a distress rating level. In Fig. 7(c), it can be observed that the extent

of staining seems fairly large; however, because the damage is only
 superficial (aesthetic only) and not “erosion,” the deterioration
 component under the assigned code is selected as “ACID-ERO-
 MIN-G.” Moreover, because of a lack of a more suitable code
 in this existing study, “acid attack” has been selected as the primary
 mechanism. This results in a structural damage condition index of
 2.33. Because the bridge does not have any other degradation, the
 criticality of damage in the bridge structure is deemed minimal.

Similarly, for the condition assessment of the storage structure,
 a series of photographs are taken. The building is divided into
 four elements; north side, east side, west side and south side walls.



F9:1 **Fig. 9.** South side wall of storage building: (a) unprocessed images; (b) corresponding distress-identified images; (c) effect for each deterioration;
 F9:2 (d) overall damage index

533 Fig. 8(a) shows a real image of the outside and inside walls of the
 534 selected elements. The north side wall is not considered in this
 535 study; it is free from any deterioration because it was covered by
 536 asbestos cement roofing sheets. RGB images are fed into the GUI
 537 tool to detect the various distresses. Fig. 8 shows the corresponding
 538 distress identified for the east wall element based on the developed
 539 algorithms. These RGB images and distress-identified images will
 540 be used further to select the associated distress codes, which in turn
 541 evaluate the condition index for the east side wall element, which
 542 is found to be 3.74. Similarly, the condition index is calculated
 543 for other walls, as shown in Figs. 9 and 10. SCI considering equal
 544 weights for all the elements is calculated as 3.68, as given in
 545 Table 2, based on the average weighted method that signifies the
 546 criticality of the structure. According to the evaluated SCI, it can be
 547 said that the building has the medium damage condition. The entire
 548 storage building has been evaluated by considering the condition of

each wall (individual MF), and then the overall combined effect of
 all the walls is considered. As can be seen, the individual wall has
 a condition rating of approximately 3 and more (because the cracks
 have a more severe damage condition rating than the surface
 deterioration), and the combined condition of all the walls turned
 out to be 3.68.

Conclusion

A GUI tool for rapid estimation of damage indices of civil infra-
 structure is developed. The formulated protocol uses image func-
 tionalities and fuzzy sets to ascertain several structural distresses.
 Diverse imaging strategies are incorporated to accomplish detec-
 tion and quantification of structural defects and also to provide
 a comprehensive evaluation of civil structures. In crack detection,

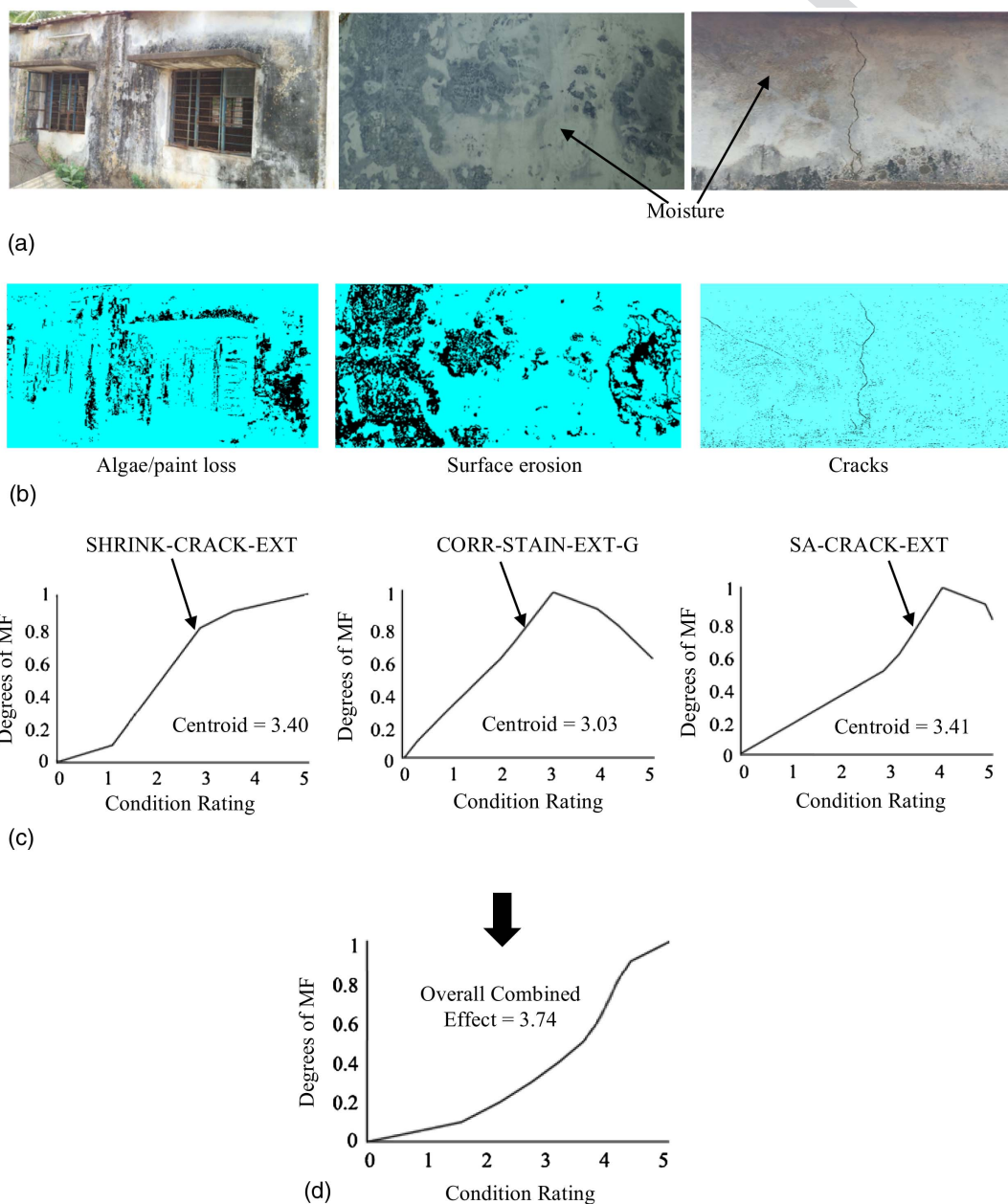


Fig. 10. West side wall of storage building: (a) unprocessed images; (b) corresponding distress-identified images; (c) effects for each deterioration; (d) overall damage index

17 Table 2. SCI for the Storage Building

T2:1	Element name	Element weight	Assigned codes	SCI because of each deterioration mechanism	Combined SCI for each element	Combined SCI for the structure
T2:2	East wall	1	SHRINK-CRACK-EXT	3.40	3.74	3.68
T2:3			CORR-STAIN-EXT-G	3.03		
T2:4			SA-CRACK-EXT	3.41		
T2:5	South wall	1	SHRINK-CRACK-EXT	3.40	3.56	
T2:6			CORR-STAIN-EXT-G	3.03		
T2:7	West wall	1	SHRINK-CRACK-EXT	3.40	3.74	
T2:8			SA-CRACK-EXT	3.41		
T2:9			CORR-STAIN-EXT-G	3.03		

562 BHT yielded an average error of 5% in comparison with HSV.
 563 The surface degradation is effortlessly appraised with the HSV
 564 and grayscale thresholding methodologies. A simplified GUI tool
 565 is developed in a *MATLAB* environment to ease the assessment
 566 of structures. Case studies are presented to examine the level of
 567 deterioration. Results reveal that the evaluated bridge attained 2.33
 568 and the storage building 3.68 as the damage index, which signifies
 569 the criticality of damage of each structure. In the future, robust sensor
 570 modules such as infrared thermal imaging and stereo mapping
 571 can be integrated for enhanced data acquisition and structural as-
 572 sessment. This inclusion provides sophisticated hardware-cum-
 573 software utility for rapid and effective evaluation of bridges, dams,
 574 monuments, buildings, and other structural members.

$$\text{If } \left[R_i < 0.1 \times \left(\sum_{i=0}^5 R_i \right) \right]$$

then update $[R_i = 0]$

3. The obtained numbers are then normalized as 580

$$\mu_{xi} = \frac{R_i}{\max_{i=0,1,2,\dots,5}(R_i)}$$

4. The resulting numbers are shown in Table 4 after tuning; and 581
 5. The obtained MFs are modified using linguistic hedges or modi- 582
 fiers (Mitra et al. 2010) to account for local and global levels of 583
 defects, which are given by 584

575 Appendix. Procedure for the Development of MFs

- 576
 577 1. Collect the data from experts or visual inspectors. Table 3 shows
 578 the summary of expert responses used in this study;
 579 2. Further tune the data as per the following equations:

If $[R_i < R_{i-1} \text{ and } R_i < R_{i+1}]$,
 then update $[R_i = 0.5(R_{i-1} + R_{i+1})]$

Local: $\mu_{x_i,local} = \mu_{x_i}^{1/2}$ for $x_i \leq x_0$
 $\mu_{x_i,local} = \mu_{x_i}^2$ for $x_i \geq x_0$

Global: $\mu_{x_i,global} = \mu_{x_i}^2$ for $x_i \leq x_0$
 $\mu_{x_i,global} = \mu_{x_i}^{1/2}$ for $x_i \geq x_0$

and

where x_i = condition rating (0–5); and x_0 = condition rating
 where MF is maximum. 585

Table 3. Summary of the Expert Responses for Various Distress Conditions (Data from Jain and Bhattacharjee 2012b)

T3:1	Type of defects because of corrosion	Distress state description	Assigned rating and number of responses					T3:2
			0	1	2	3	4	
T3:3	Spalling	Depressions less than 20 mm in depth and not exceeding 150 mm in any other dimension	1	5	10	19	10	4
T3:4		Depressions of size more than 20 mm in depth with any other dimension greater than 150 mm	0	1	4	9	21	14
T3:5	Rust staining and moisture marks	Stains visible in isolated patches	10	12	19	8	2	0
T3:6		Stains visible covering large area	2	8	11	14	11	5
T3:7	Cracks	Crack parallel to either stirrups or longitudinal rebars or main rebars, running in one direction only (1D cracks)	1	9	11	16	10	4
T3:8		Isolated cracks parallel to both stirrups or longitudinal rebars and main rebars (2D cracks)	0	3	14	15	15	4
T3:9		Extensive cracks, spanning in both directions, over relatively large surface area	0	0	4	10	17	20

Note: The following condition rating definitions are considered (based on repair priority). 0: Condition does not require any repair. 1: Very low-priority repair; can be delayed for long span of time. 2: Low-priority repair; actions may be delayed for significant time. 3: Medium-priority repair; actions may be delayed for some time. 4: High-priority repair; urgent actions might be required. 5: Condition is critical; actions must be carried out immediately.

Table 4. Summary of Obtained Condition Indices Based on the Distress State

	Type of defects because of corrosion	Distress state description	Condition indices					T4:2	
			0	1	2	3	4		5
T4:1	Spalling	Depressions less than 20 mm in depth and not exceeding 150 mm in any other dimension	0.05	0.26	0.53	1.00	0.53	0.21	
T4:4		Depressions of size more than 20 mm in depth with any other dimension greater than 150 mm	0.00	0.05	0.19	0.43	1.00	0.67	
T4:5	Rust staining and moisture marks	Stains visible in isolated patches	0.53	0.63	1.00	0.42	0.11	0.00	
T4:6		Stains visible covering large area	0.14	0.57	0.79	1.00	0.79	0.36	
T4:7	Cracks	Crack parallel to either stirrups or longitudinal rebars or main rebars, running in one direction only (1D cracks)	0.06	0.56	0.69	1.00	0.63	0.25	
T4:8		Isolated cracks parallel to both stirrups or longitudinal rebars and main rebars (2D cracks)	0.00	0.20	0.93	1.00	1.00	0.27	
T4:9		Extensive cracks, spanning in both directions, over relatively large surface area	0.00	0.00	0.20	0.50	0.85	1.00	

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